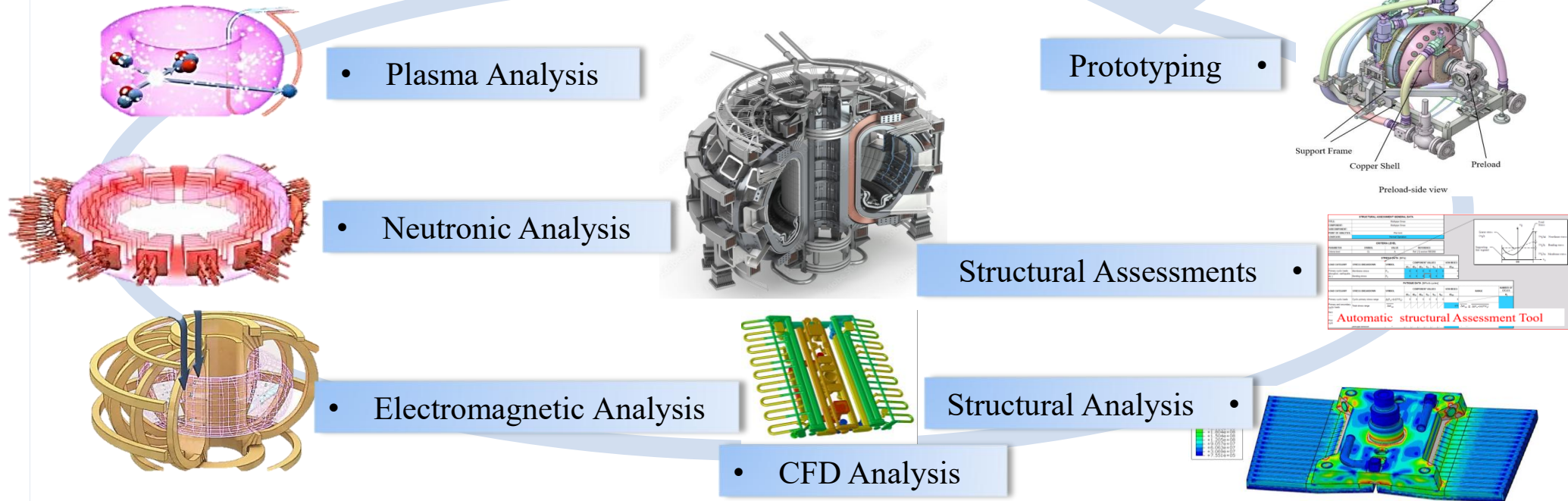




Your Partner in Computer Aided Engineering
Since 1996

Your Way To Fusion Machine

Through our complete set of Design Advisory Services



*Thanks to more than 28 years of experience and collaboration in Fusion Machines like ITER, DEMO, W7X, JET, DTT, FTU, STEP and ..., LTCalcoli has a demonstrated capability of assisting the design of a fusion machine by proposing design modifications to solve electromagnetic and structural issues, verifying the Fusion Machine design according to standards using **automatic internally developed design tools** and address toward prototypes.*

CAE Solutions

- Electromagnetic Analysis
- Electro-mechanical analysis
- Plasma Disruption with MAX FEA
- Structural mechanics
- Thermal analysis
- Thermo-structural analysis
- Fluid dynamics (CFD)
- Vibroacoustic
- Fatigue analysis
- Fracture Mechanics
- Elasto-Plastic Analysis

Design Solutions

- Structural integrity studies according to SDC-IC, ASME and RCC-MR.
- Engineering consultancy from design to prototype
- Design by Analysis
- Design by Rule

Trainings

- Finite Element Method Theories
- Simulia Abaqus
- Ansys Workbench
- Ansys APDL
- Hypermesh

LTCalcoli has an established experience in the design by analysis of Thermo-Nuclear Fusion Reactors from a strong and long-term collaboration with:

- ✓ ITER Organization
- ✓ ENEA (Italian National Agency for New Technologies, Energy and Sustainable Economic Development):
 - FTU (Tokamak Upgrade)
 - FAST
 - DTT
 - IGNITOR
- ✓ W7-X IPP
- ✓ STEP (in Consortium with IDOM UK)
- ✓ EUROfusion Program:
 - DEMO
 - VNS
- CEA - WEST
- ✓ JET
- ✓ MaritimeFusion
- ✓ CNR ISTP (the Italian National Research Council Institute for Plasma Physics)

90% of LTCalcoli revenue is coming from contracts on Fusion Machines



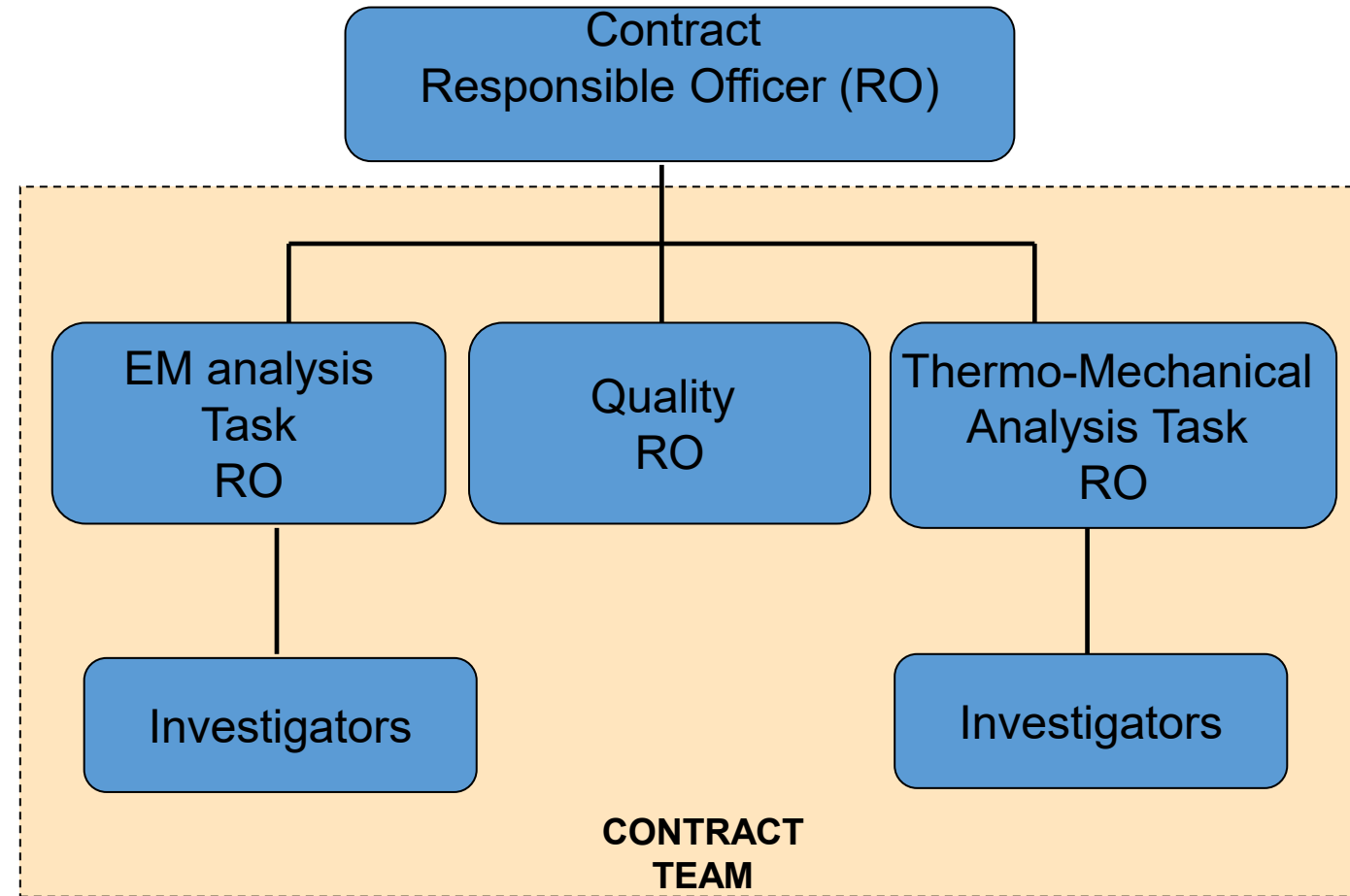
Certifications

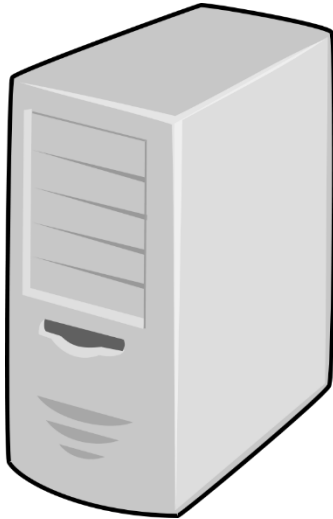


Each **Contract** has its “reference numerical code”, used for each communication with Customer (mail, presentation, report ..)

Each **Data** referred to the Contract is stored in the “Referenced Code” area

Each **Computer** and each **Computational Server** is backed up every night into the storage servers





Servers

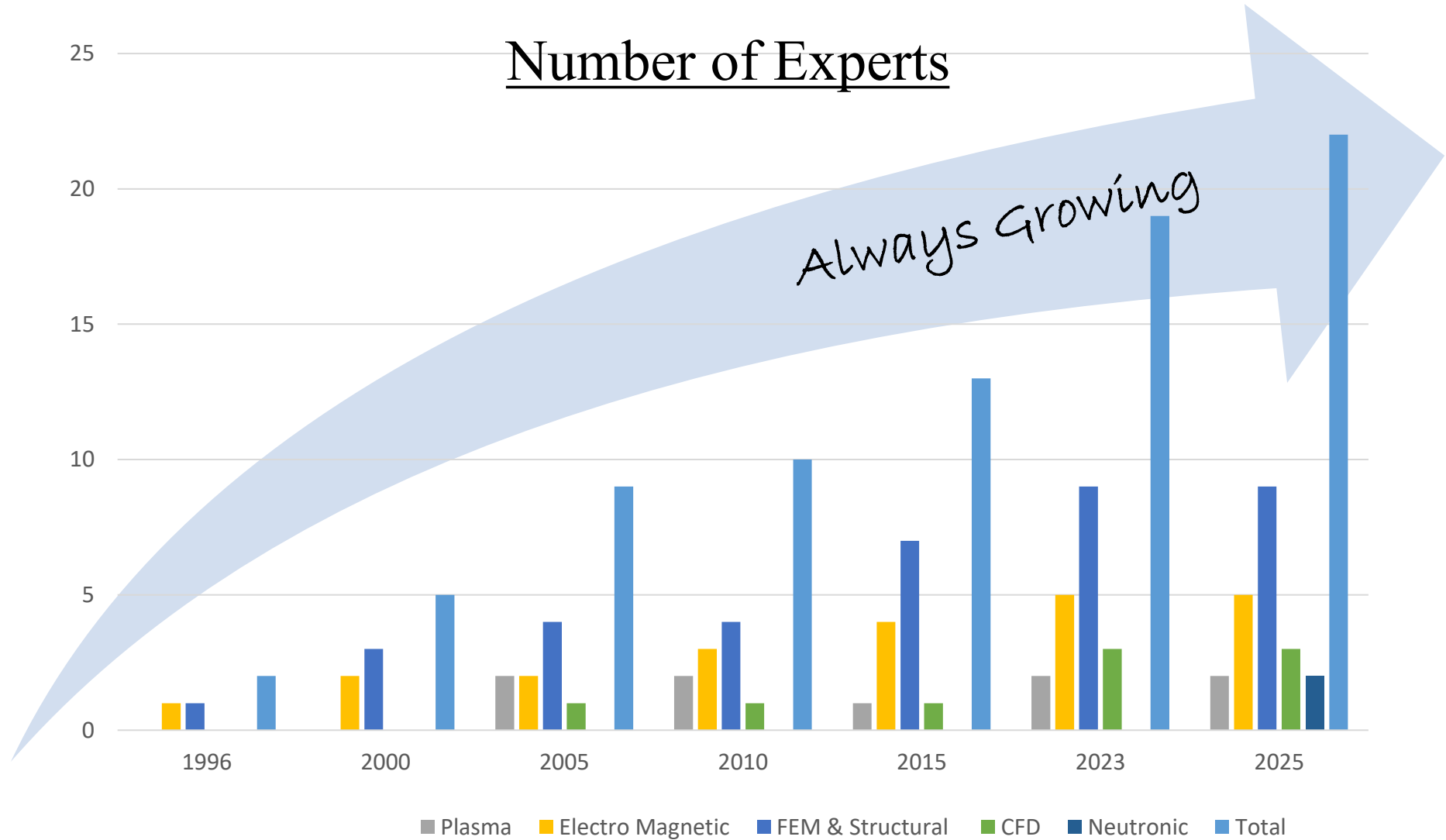
- #1 DELL 64 Cores – 768 Gb RAM
- #1 DELL 48Cores – 768 Gb RAM
- #1 HP 24 Cores – 720 Gb RAM
- #1 HP 24 Cores – 520 Gb RAM
- #1 DELL 32 Cores - 128 Gb RAM
- #1 DELL 24 Cores – 192 Gb RAM
- #3 Storage servers for data managing

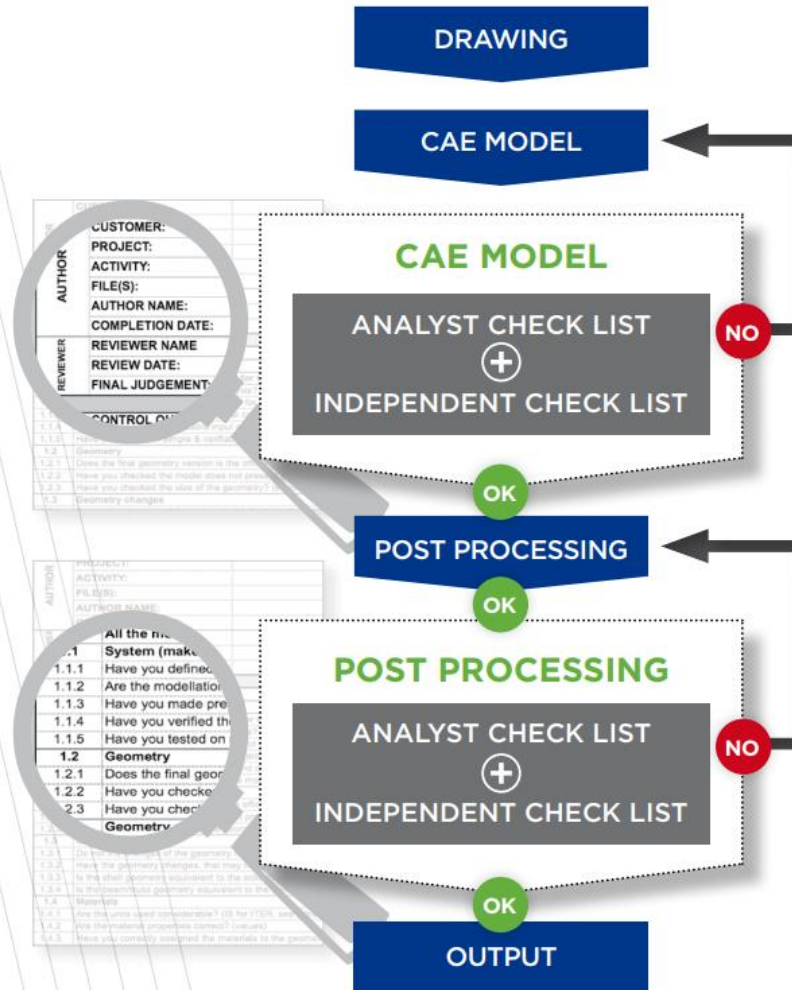


Softwares

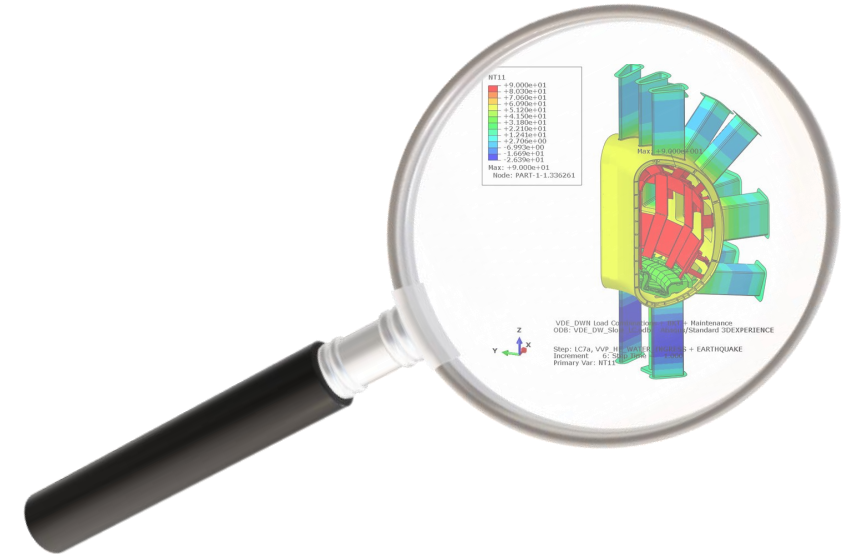
- DS/Simulia (ABAQUS)
- ANSYS/Mechanical
- ANSYS/Fluent
- MSC
Nastran/Patran/ADAMS/MARC
- Altair Hypermesh
- Intel Fortran
- Matworks Matlab
- CATIA V5

Resources





- Any task will go through quality control procedure at different levels of activity.
- At each level the task will be controlled at least by two investigators. One analyst investigator and one independent investigator





All the power of Virtual Prototyping on Cloud Application

Copyright © 2012. LTCalcoli srl

Optimize the product by yourself in 3 steps:

STEP 1 Choose your model



STEP 2 Insert your parameters



STEP 3 View your results



Benefits

- Minimizing model optimization cost
- Benefiting from super-computing infrastructure while paying only for the effective use
- Saving time acting directly on the calculation model
- Updating the results easily by changing the pre-defined parameters
- No need for FEM knowledge
- Reducing time to market



(11) EP 2 757 495 A1

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:
23.07.2014 Bulletin 2014/30

(51) Int. Cl.:
G06F 17/10 (2006.01)

(21) Application number: 14151934.8

(22) Date of filing: 21.01.2014

(84) Designated Contracting States:
AL AT BE BG CH CY CZ DE DK EE ES FI FR GB
GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO
PL PT RO RS SE SI SK SM TR
Designated Extension States:
BA ME

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(30) Priority: 22.01.2013 IT GE20130008

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(54) System for parameterized finite element analysis

(57) A Finite Element Modeling (FEM) system, providing Finite Element Analysis (FEA) for numerical modeling of physical systems in a variety of engineering disciplines, comprising means for generating a finite element model, data processing means, result delivering means for delivering the results so obtained to a user,

wherein the finite element model generated is further parameterized, and a user interface is provided for changing the parameters of the finite element model and for entering such parameters into said data processing means.

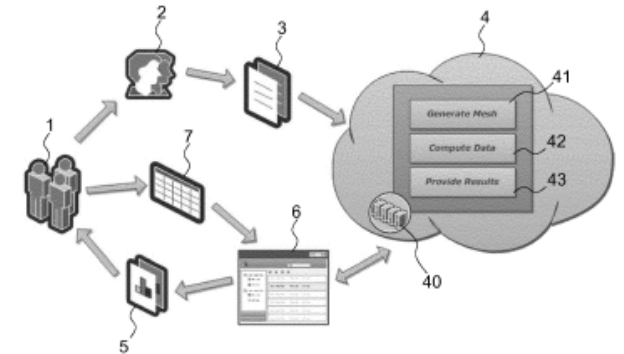


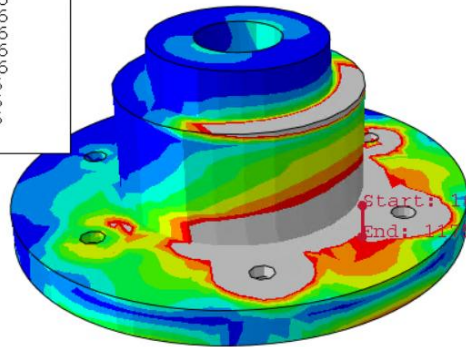
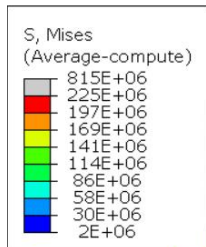
Fig 2

EP 2 757 495 A1

Printed by Jouve, 75001 PARIS (FR)

Automated Tools for performing structural assessments

Automated Tools



STRUCTURAL ASSESSMENT GENERAL DATA

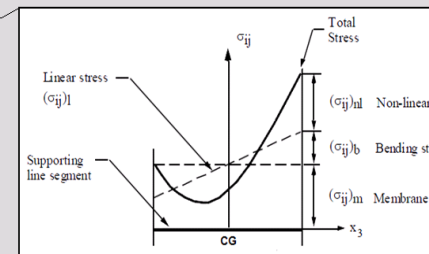
7	Multipipe Smax	
	Multipipe Smax	
	Plot limit	
	Normal Operation	
CRITERIA LEVEL		
SYMBOL	VALUE	REFERENCE
CL	A	Ref. [1] section RB3260

STRESS DATA [MPa]

LOAD CATEGORY	STRESS BREAKDOWN	SYMBOL	COMPONENT VALUES							VON MISES
			σ_{11}	σ_{22}	σ_{33}	τ_{12}	τ_{13}	τ_{23}		
Primary cyclic loads: Membrane stress	Membrane stress	P_m	0	0	0	0	0	0	0	0
Primary cyclic loads: Bending stress	Bending stress	P_b	0	0	0	0	0	0	0	0

FATIGUE DATA [MPa & cycles]

LOAD CATEGORY	STRESS BREAKDOWN	SYMBOL	COMPONENT VALUES							VON MISES	RANGE	NUMBER OF CYCLES
			σ_{11}	σ_{22}	σ_{33}	τ_{12}	τ_{13}	τ_{23}				n_i
Primary cyclic loads	Cyclic primary stress range	$\Delta(P_m + 0.67 \cdot P_b)$	0	0	0	0	0	0	0	0		
Primary and secondary cyclic loads	Total stress range	$\Delta\sigma_{tot}$								573	$\Delta\sigma_{tot} \geq \Delta(P_m + 0.67 \cdot P_b)$	



STRUCTURAL ASSESSMENT GENERAL DATA:

TITLE: Equatorial Port Plug # 02 SUBCOMPONENT: Path 1
COMPONENT: Port Plug Body POINT OF ANALYSIS:

ENVIRONMENTAL CONDITIONS:

Temperature T = 70 [°C]

LOADING DATA: LC#01

Criteria level CL = A [adim.]
Primary membrane stress intensity \bar{P}_m = 110 [MPa]
Primary membrane plus bending stress intensity $\bar{P}_L + \bar{P}_b$ = 199 [MPa]

ALLOWABLE DATA (stress intensity):

Allowable primary membrane S_m = 147 [MPa]
Bending shape factor K = 1.50 [adim.]

STRUCTURAL ASSESSMENTS:

RB3251.11 Rules for prevention of P-type damage - Elastic analysis

$$SM = \frac{S_m}{\bar{P}_m} = \frac{147 \text{ [MPa]}}{110 \text{ [MPa]}} = 1.33$$

$$SM = \frac{K \cdot S_m}{\bar{P}_L + \bar{P}_b} = \frac{221 \text{ [MPa]}}{199 \text{ [MPa]}} = 1.11$$

Automatic report generation

Automatic structural Assessment Tool

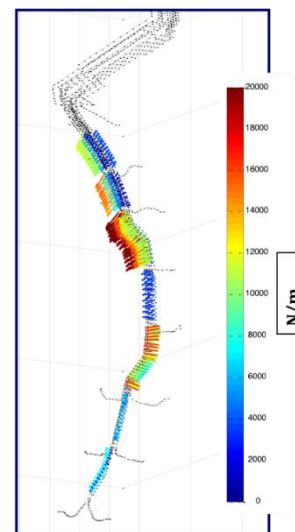
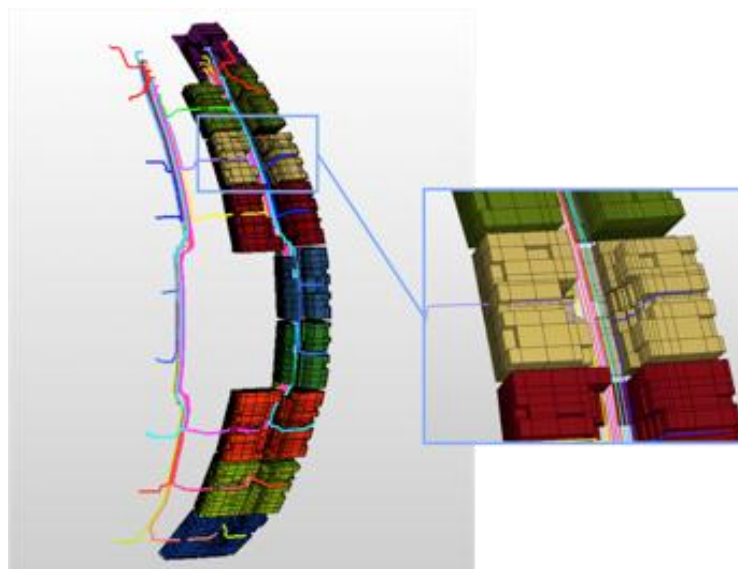
EM Wire Element in Ansys

The “**EM wire element**” are developed for the evaluation of eddy currents on in-Vessel and Out-Vessel pipes avoiding the use of solid elements in electromagnetic analysis

LTCalcoli has developed and introduced into Ansys EM code the “**EM wire element**” defined as “grid to grid” element for the EM modelling of pipe, see picture below, used for the evaluation of the EM loads on pipes, avoiding the use of solid elements in electromagnetic analysis.

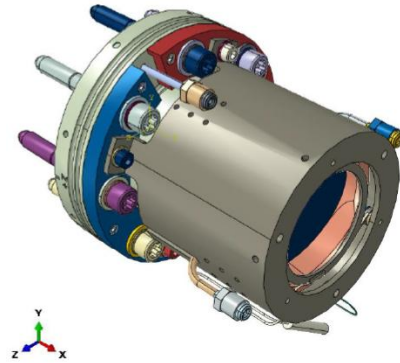
The evaluation of the EM loads acting on the pipes in general can be carried out with good accuracy by assimilating the to 1-dimensional conductors with electrical properties equivalent to those of the pipes themselves.

Automated Tools

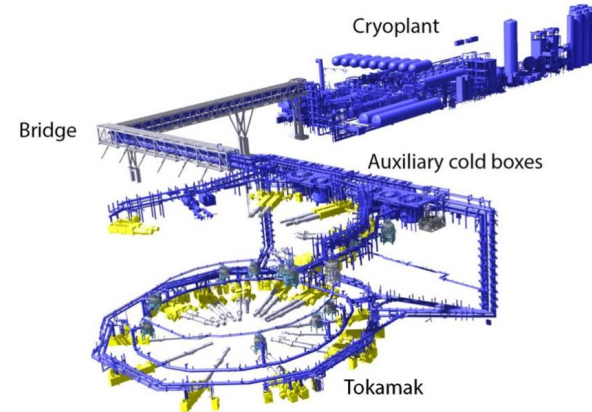


*EM-wire elements of blanket manifold
– Lorentz Forces per unit length on the
pipes modelled with “EM wire element”*

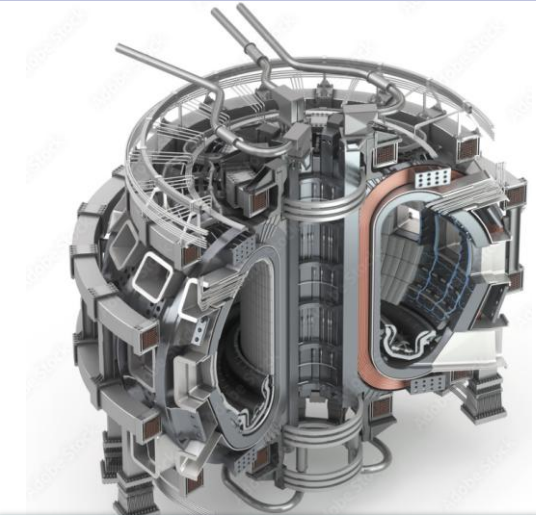
Example of Activities



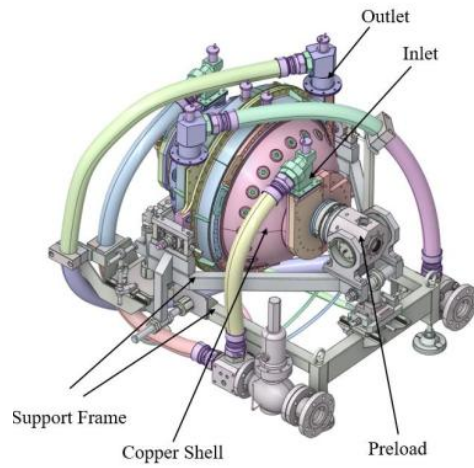
Optical Systems



Cryogenic components



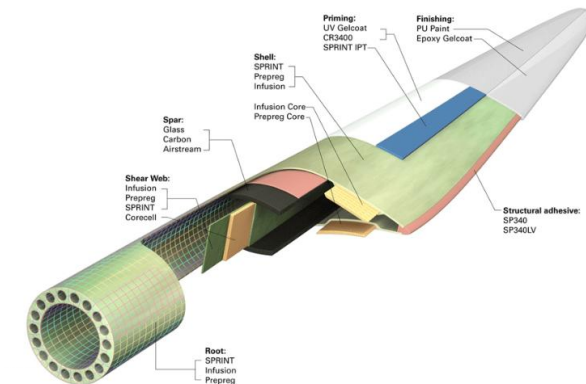
Harsh Environment components



Vacuum Systems



Thermal Insulation systems



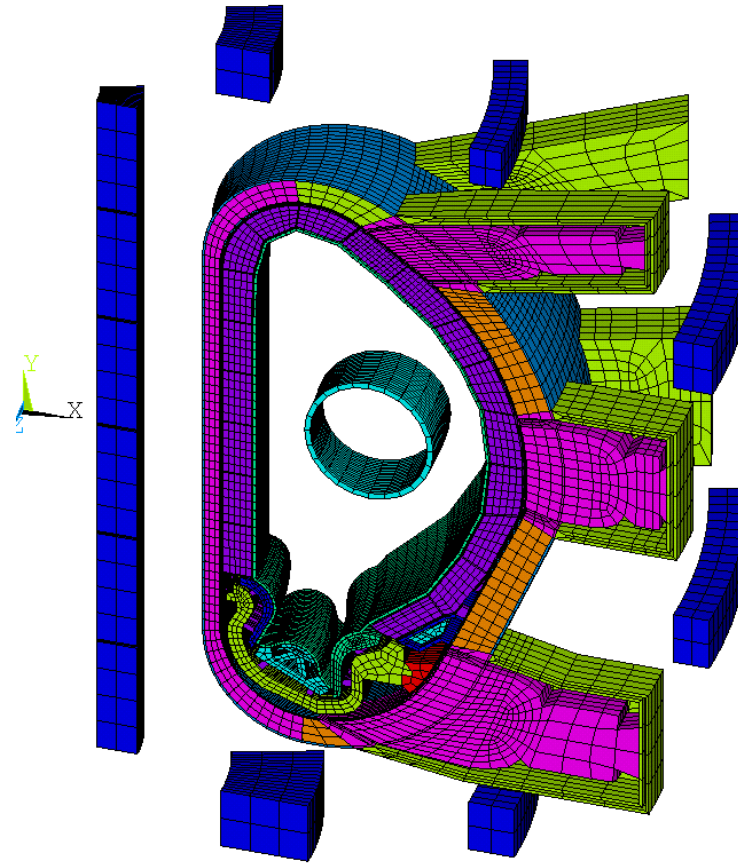
Composite Material Components

ITER Blankets EM analysis:

All the FEM realised by means of Ansys are based on the ITER EM Global Model (GM) which is a general model of the ITER VV including all the details impacting the EM loads on the in vessel components

For each BSM analysis the GM has been refined to get the needed level of detail in the region of interest

For each BSM two or three disruptions have been analysed (worst cat. II and worst cat. III)



Analysis on BM#02:

- fast DW VDE III with 36 ms lcq
- fast DW VDE II

Analysis on BM#10 FE model:

- Up Major Disruption II with 36 ms lcq
- Fast UP VDE III with 16 ms ecq

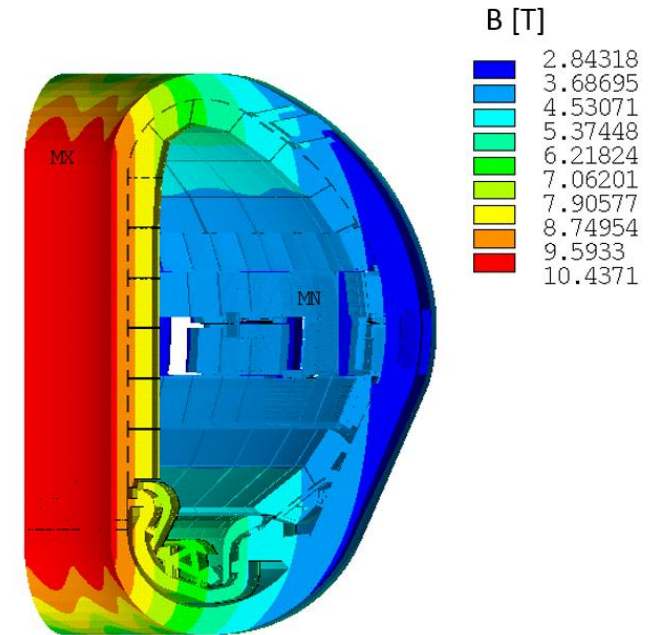
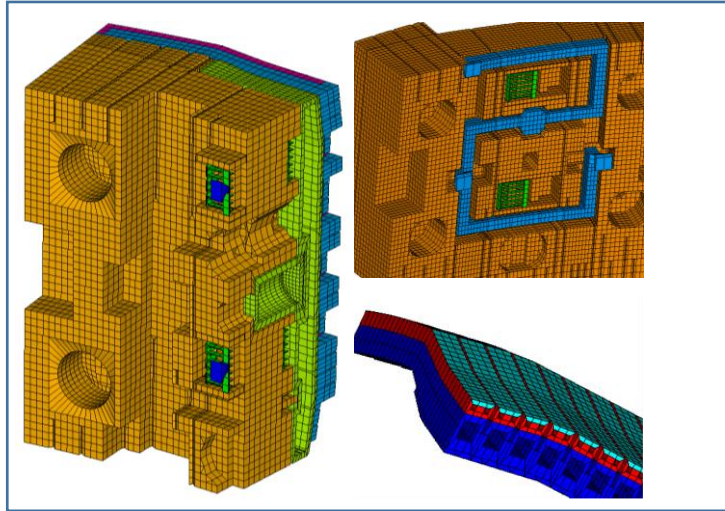
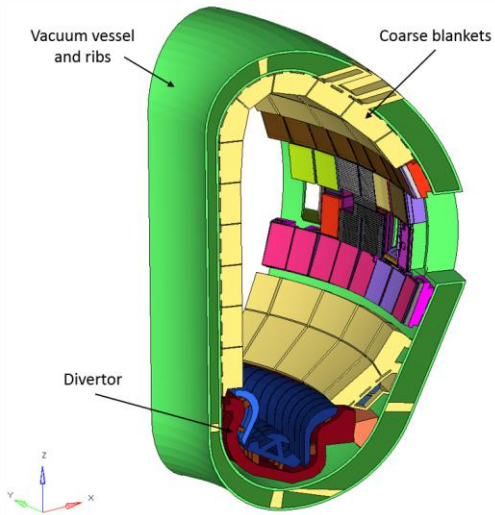
Analysis on BM#12:

- fast UP VDE III with 36 ms lcq
- fast DW Major Disruption II with 16 ms ecq

Analysis on BM#16st:

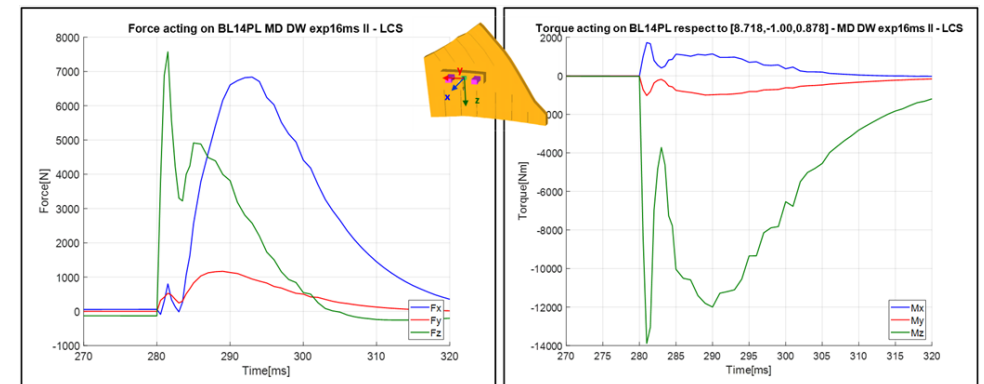
- fast DW VDE III with 36 ms lcq
- DW Major Disruption II with 16 ms ecq
- DW Major Disruption III with 16 ms ecq
- DW Major Disruption II with 16 ms ecq

A complete analysis of ITER FW 10

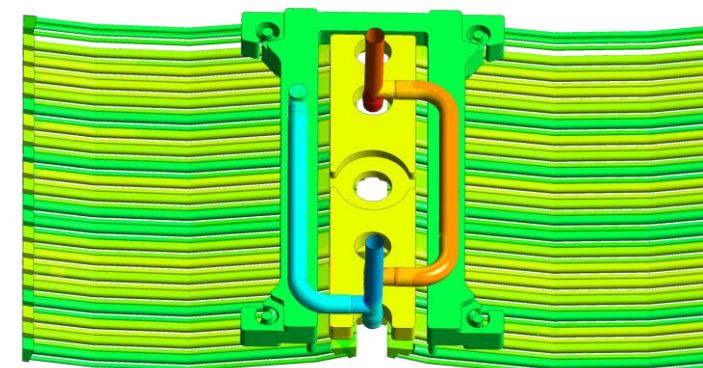
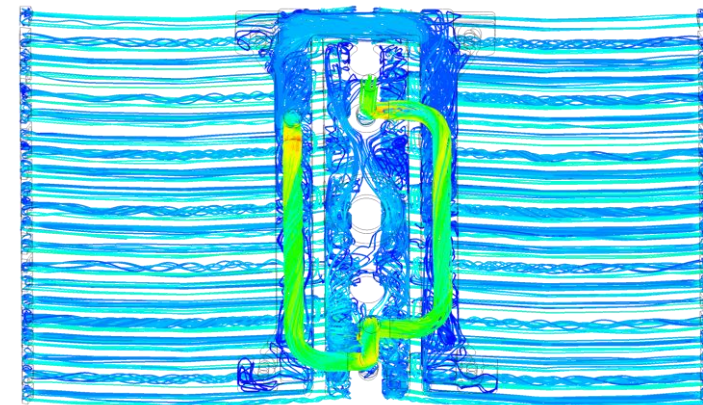
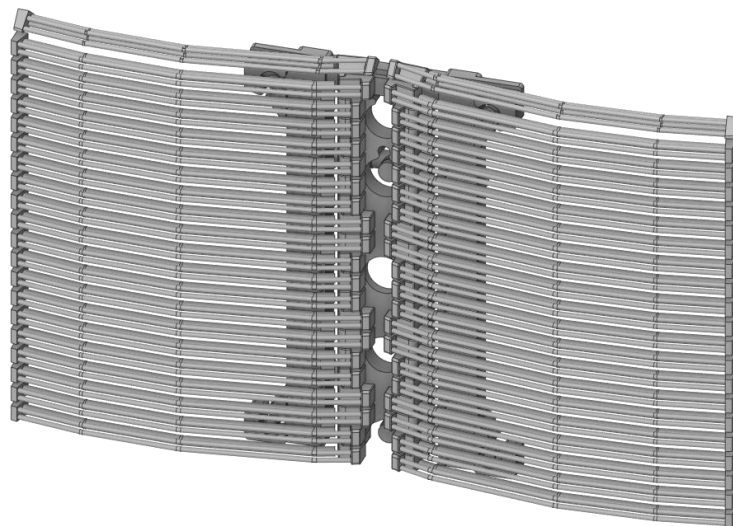
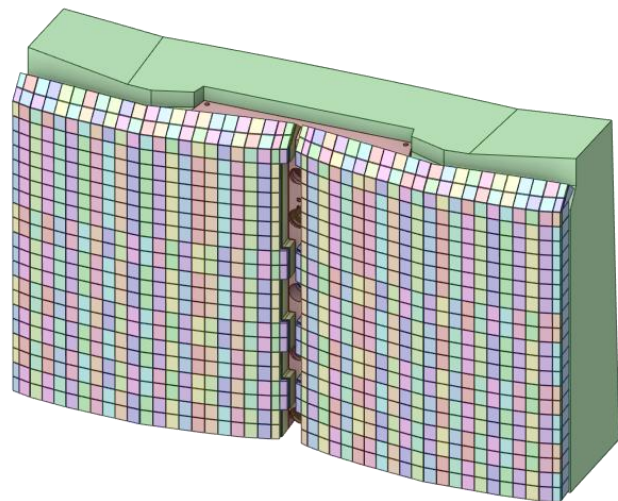


EM Analysis

- Full transient EM analysis
- Analysis of VDE / MD cat. I / cat. II / cat. III
- Computation of the Lorentz forces and ferromagnetic forces.



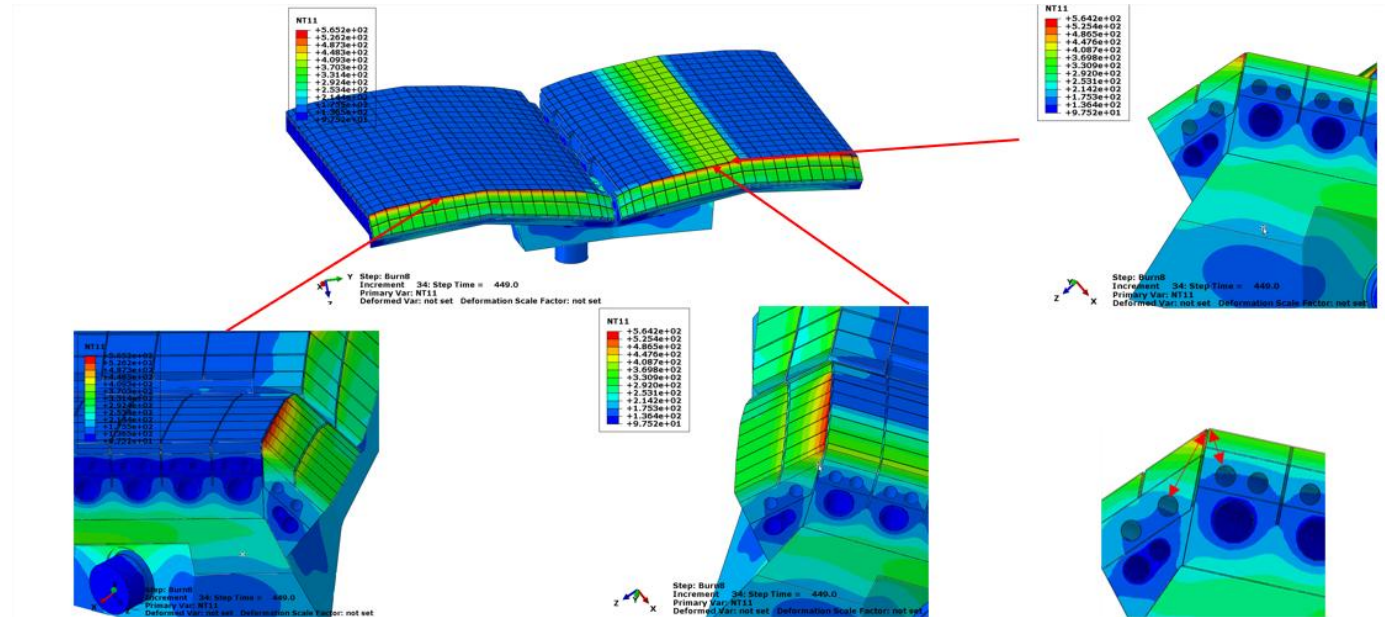
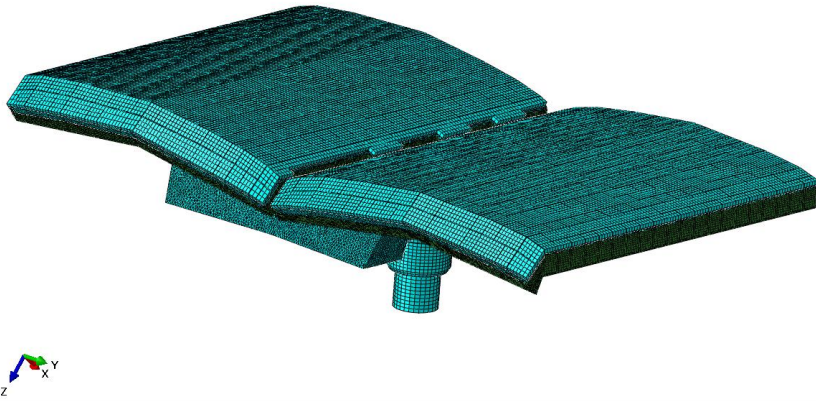
A complete analysis of ITER FW 10

**CFD Analysis**

- Steady state and full transient CFD or coupled Thermal-CFD analysis
- Mesh quality, checks and convergence criteria following the ITER best practices
- Post-processing: analysis of the pressure drop, velocity of the cooling fluid.
- Computation of Heat Transfer Coefficients (HTCs).

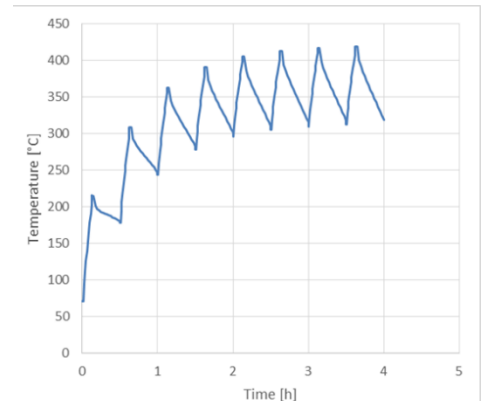
Example 2

A complete analysis of ITER FW 10

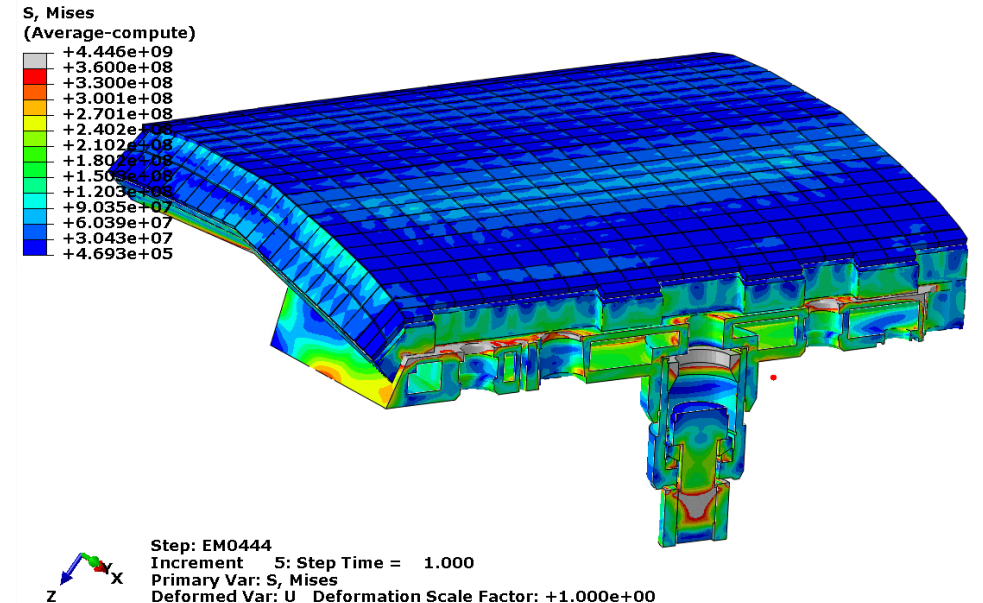
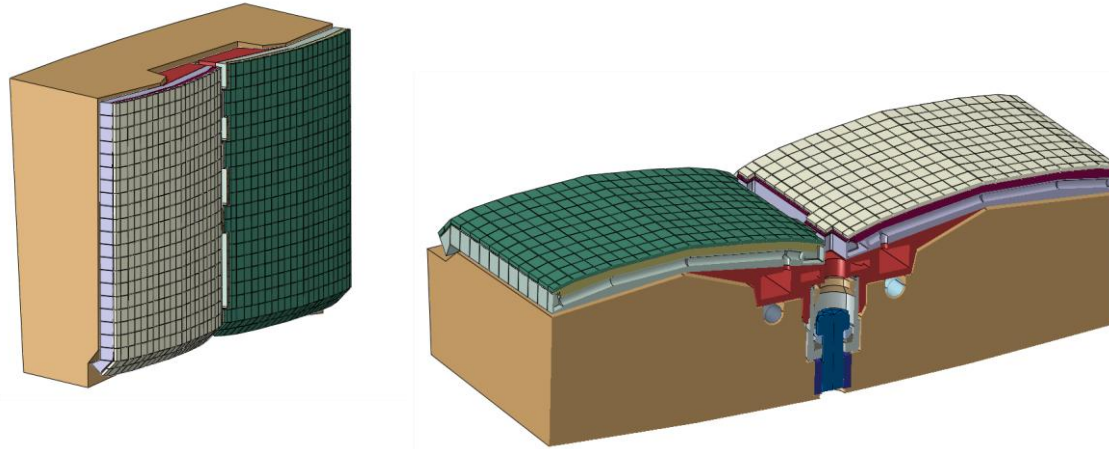


Thermal FE Analysis

- Steady state and/or full transient Thermal FE Analyses
- Mesh quality, checks and convergence criteria in accordance with ITER best practices
- Neutronic loads and Plasma flux mapping
- Estimation of the thermal contact conductivity
- Post-processing: Temperature field, time history, thermal stabilization analysis



A complete analysis of ITER FW 10



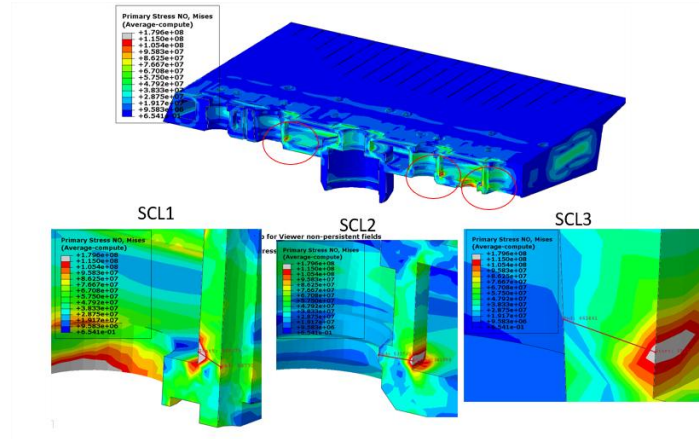
Thermo-Mechanical FE Analysis

- Non linear Static FE Analysis
- Mesh quality, checks and convergence criteria in accordance with ITER best practices
- Thermal load and EM load mapping
- Post-processing: Stresses, displacements, reactions and gap analysis
- Full transient dynamic analysis with EM load for DAF evaluation
- High quality analysis reports

A complete analysis of ITER FW 10

Structural assessments

- Structural assessments with ITER SDC-IC and Nuclear code (RCC-MR)
- Stress and load categorization
- Stress linearization
- Linear and elastic-plastic M-type static strength assessments
- Linear and elastic-plastic C-type cyclic strength assessments (fatigue and ratcheting)
- Buckling assessments
- Structural Integrity Reports in accordance with the ITER procedures



STRUCTURAL ASSESSMENT GENERAL DATA:

TITLE: ITER SUBCOMPONENT: Beam Discontinuity
COMPONENT: FW10 POINT OF ANALYSIS: Path 1

ENVIRONMENTAL CONDITIONS:

Temperature T = 360 [°C]
Neutron damage, fluence Φt = 0.00 [dpa]

LOADING DATA: LC#01

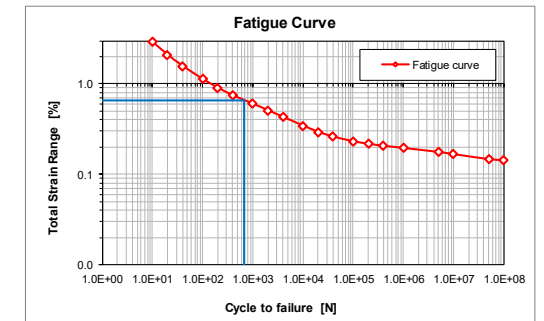
Total stress range $\Delta\sigma_{tot}$ = 1300 [MPa]
Cyclic primary stress intensity ΔP_{eff} = 0 [MPa]
Number of cycles n_f = 15000 [adim.]
Elastic strain range $\Delta\epsilon_1$ = 0.6589 [%]
Plastic strain due to primary stress range $\Delta\epsilon_2$ = 0.0000 [%]
Local plastic strain amplification $\Delta\epsilon_3$ = 0.0000 [%]
Total strain range $\Delta\epsilon_4$ = 0.0000 [%]
Linear FEM analysis $\Delta\epsilon$ = 0.66 [%]

ALLOWABLE:

Fatigue cycles N_f = 6.83E+02 [cycles]

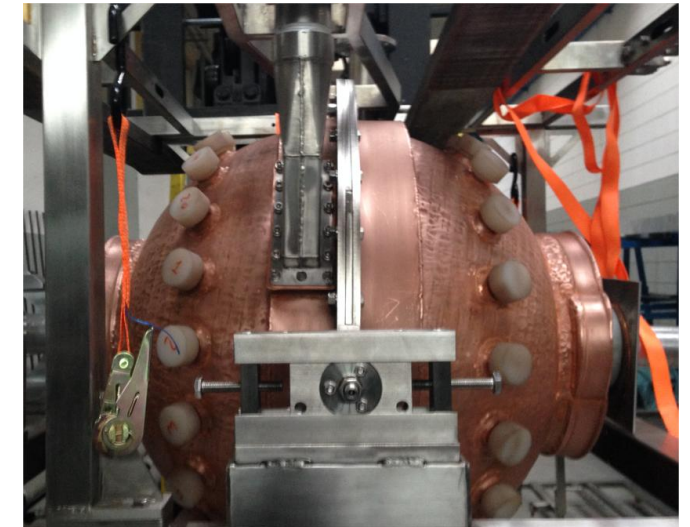
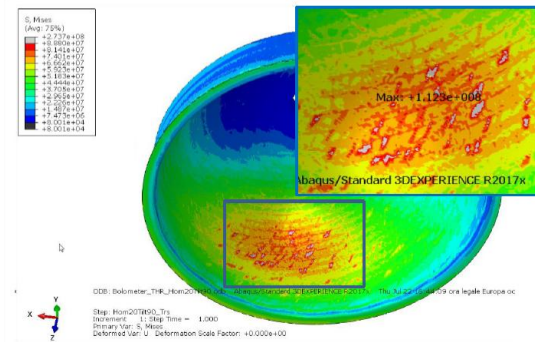
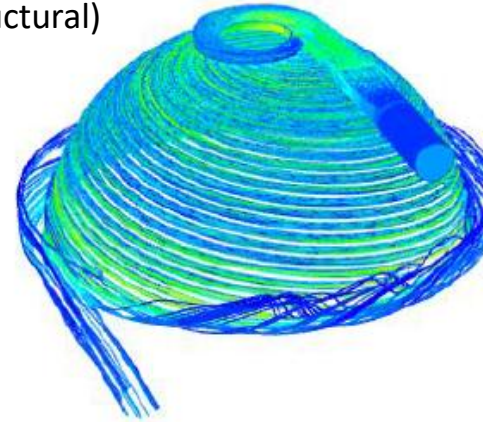
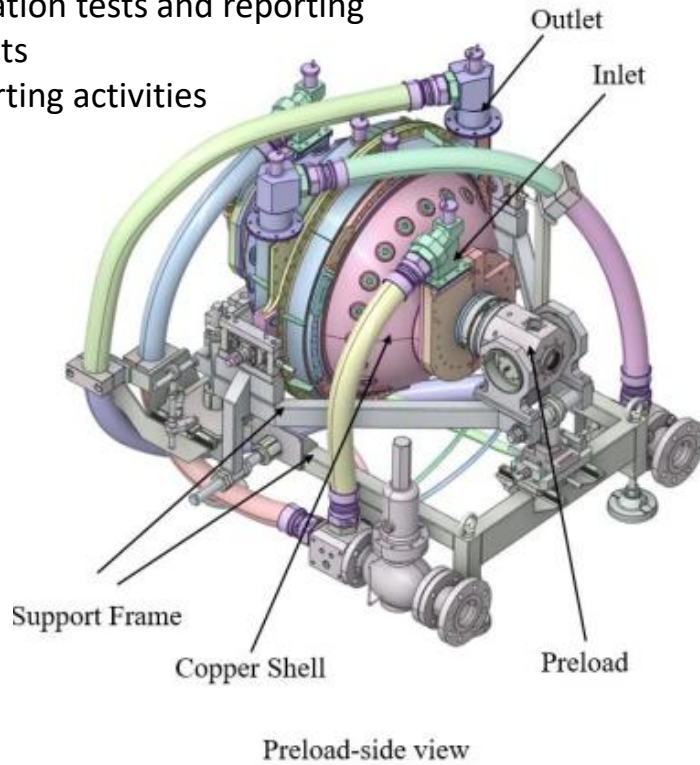
STRUCTURAL ASSESSMENTS:

Fatigue usage fraction $\frac{n_f}{N_f} = \frac{15000}{683} = 21.96$



Bolometer -Prototyping activities

- Design of the porotype (CATIA)
- Design by analysis activities (Optical, CFD, Thermal and Structural)
- Validation tests and reporting
- Patents
- Reporting activities

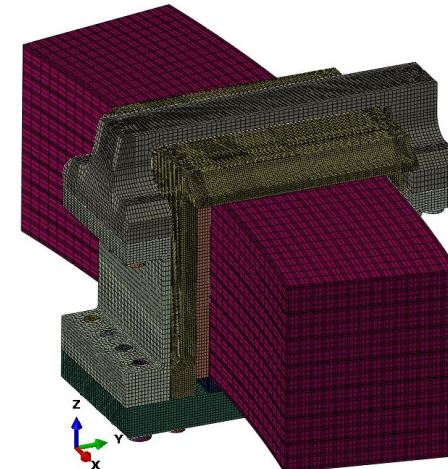
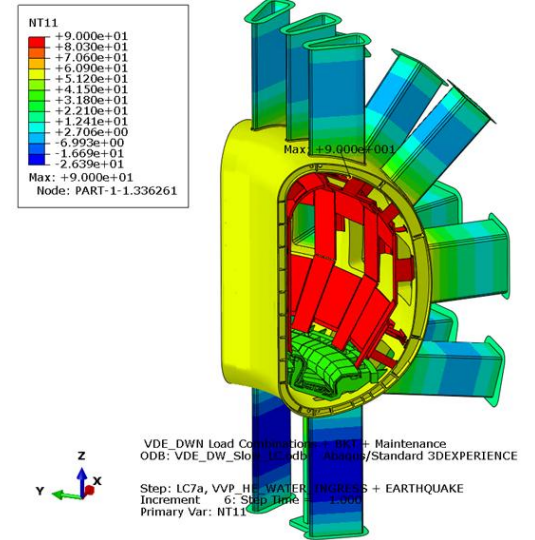
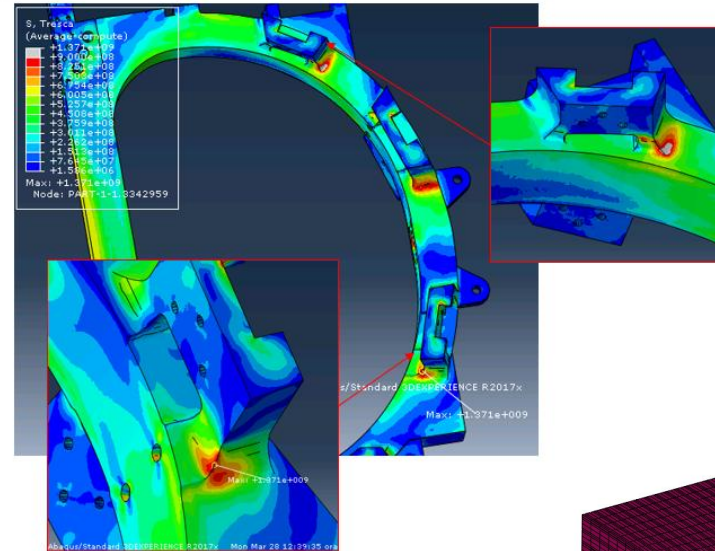
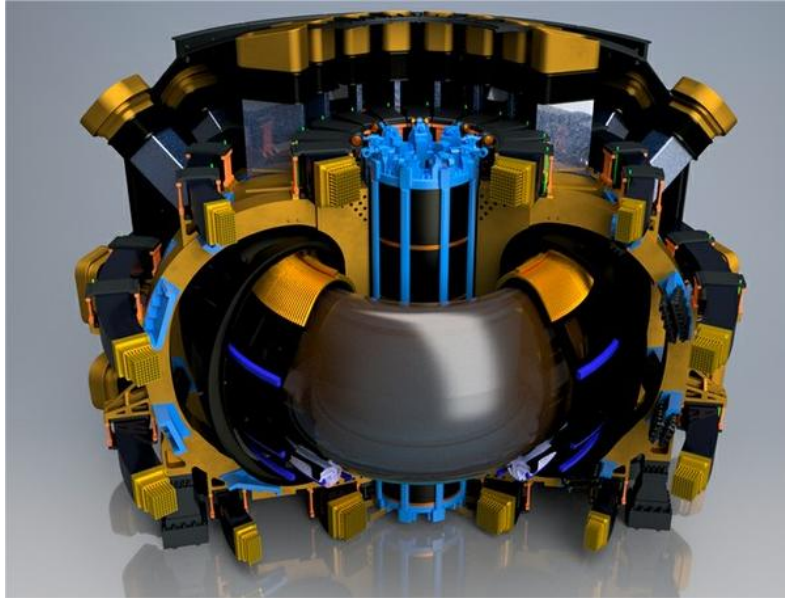


Design

Analysis

Prototype

ENEA DTT: An example of a complete Tokamak analysis

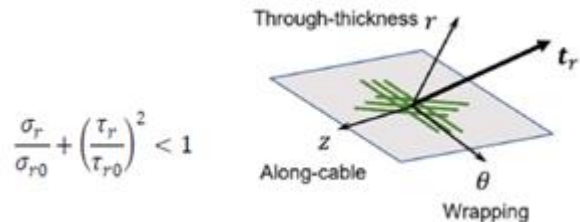
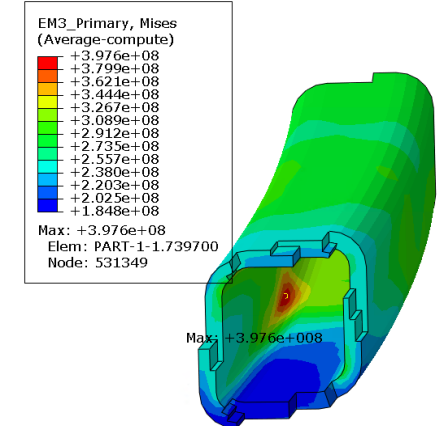
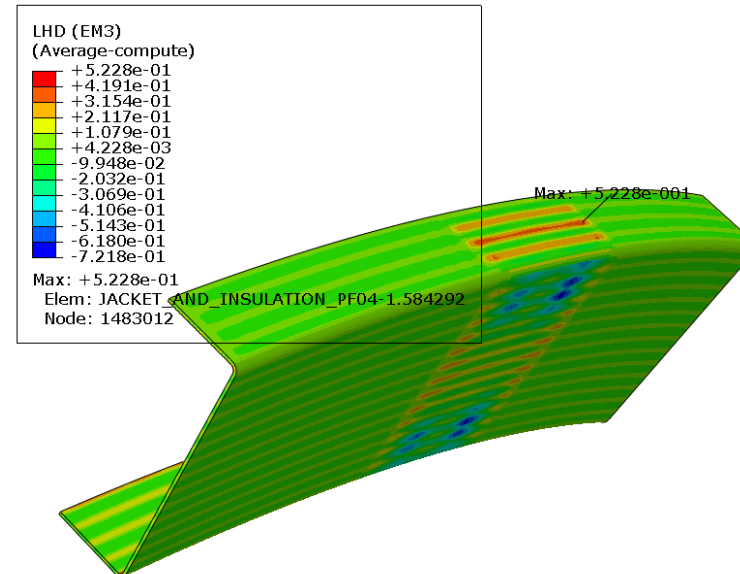
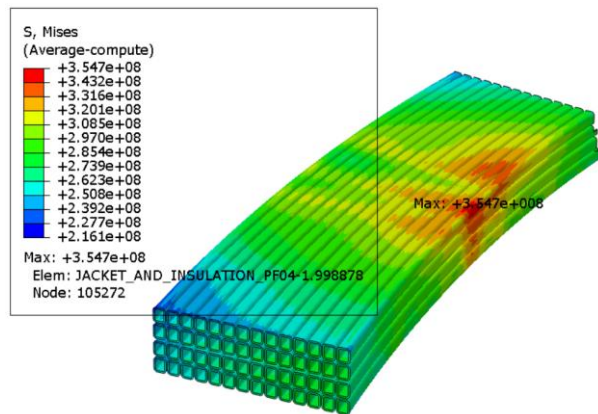


Tokamak FE analysis

- Design by analysis activities on: Toroidal coil / Poloidal Coils / Vacuum Vessel / Support / Divertor
- EM – CFD – Thermal – Structural – Seismic FE Analysis
- Independent analysis review

Superconductor Coil – structural analysis of composite materials

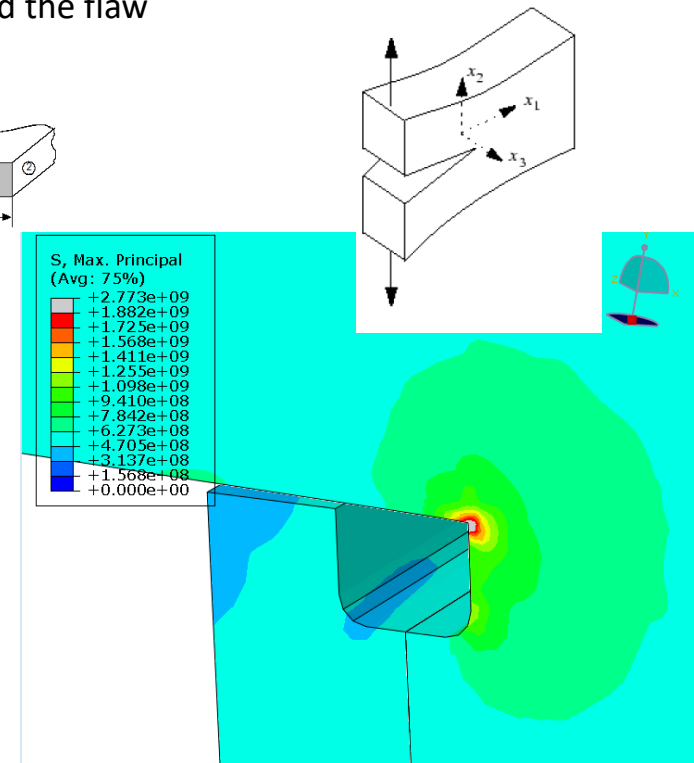
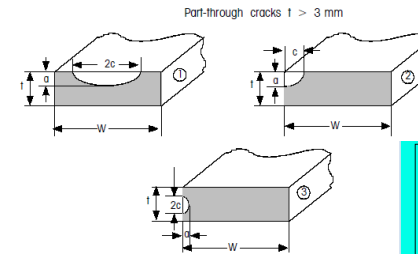
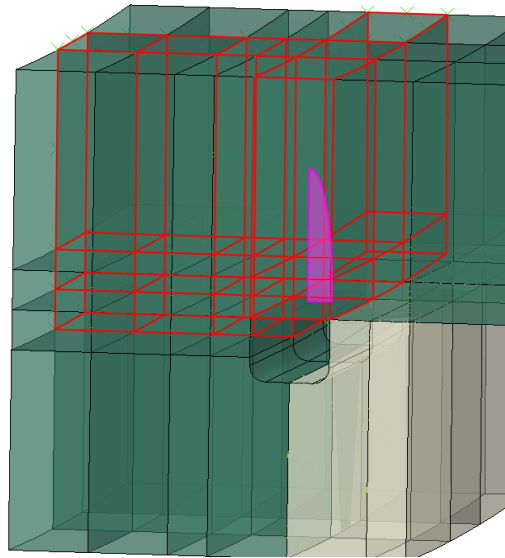
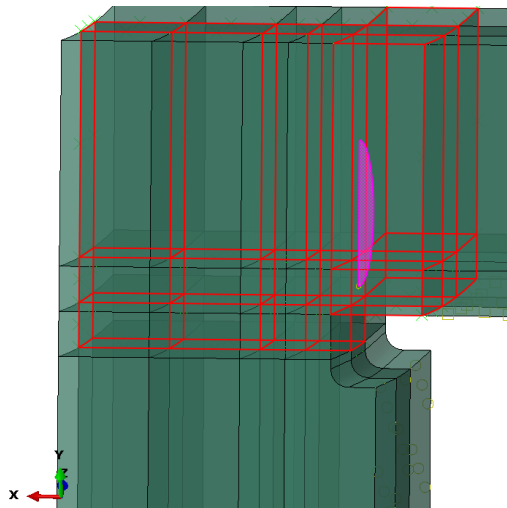
- Themo-structural analysis of a section of the Coil to verify structural strength
- Analysis with orthotropic material properties to simulate insulation layers
- Detailed analysis performed by extensively using the sub-modelling approach
- Failure Index calculated in Abaqus by considering the criterion set by the customer for this project



Fracture mechanics – structural analysis with flaws

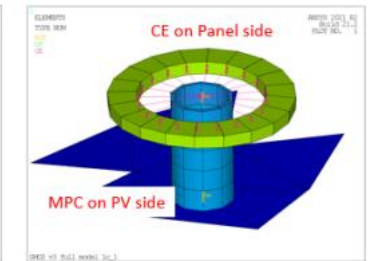
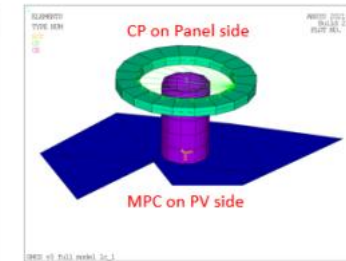
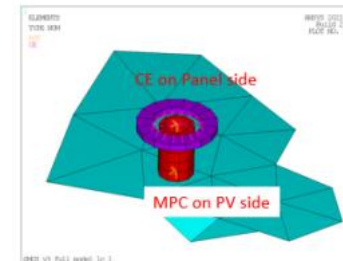
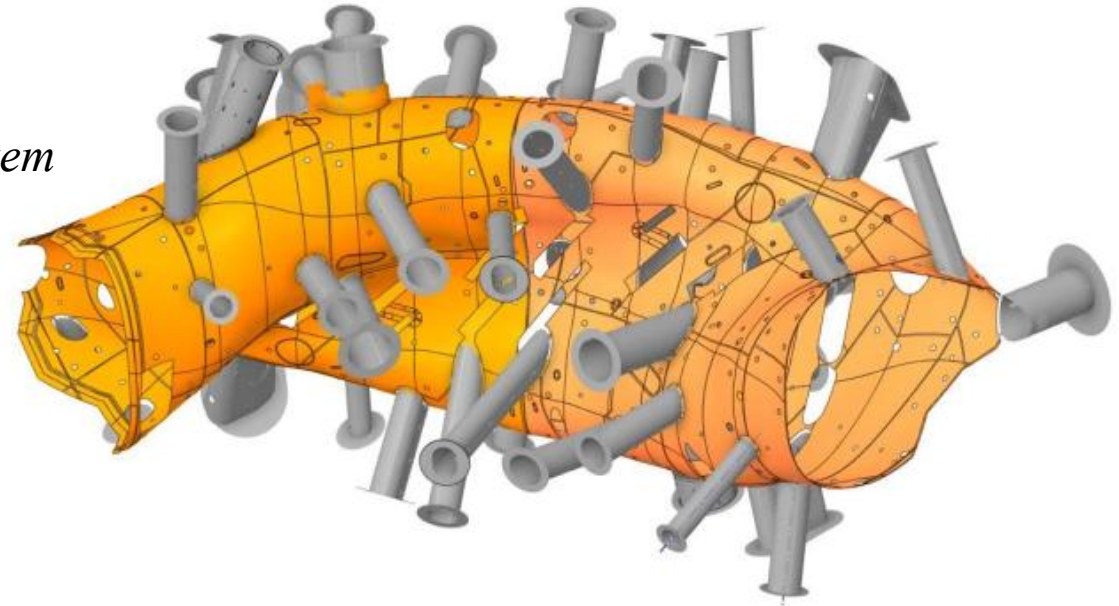
- Structural analysis of a component of fusion machine incorporating initial flaws (LEFM)
- Calculation of SIF with Abaqus XFEM approach to model corner and semi-elliptical cracks (metallic materials)
- Detailed analysis performed by extensively using the sub-modelling approach with very fine mesh around the flaw
- Verification of the component with the flaw by using handbook methods based on FEM results

Fracture Mechanics



W7-X

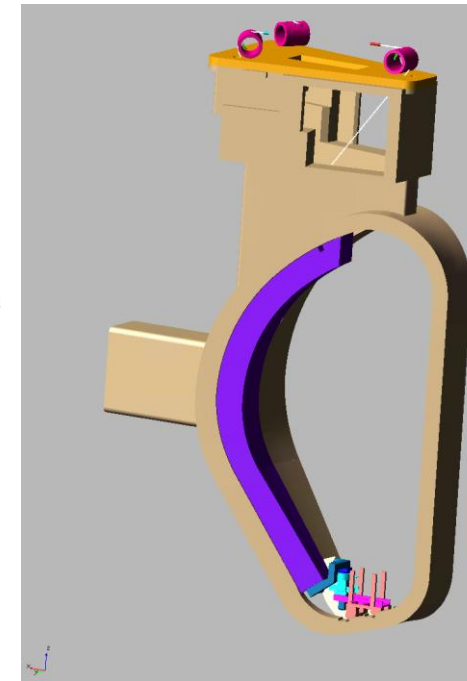
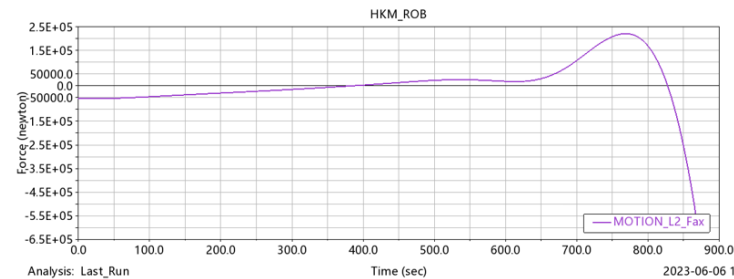
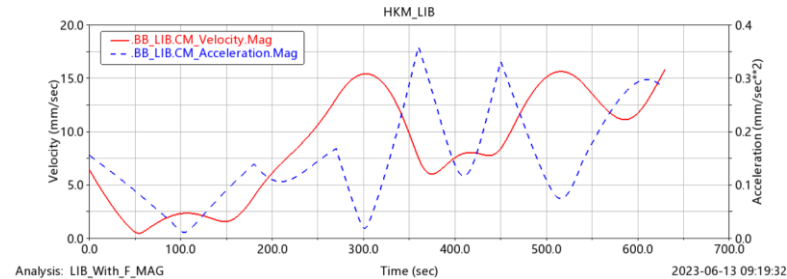
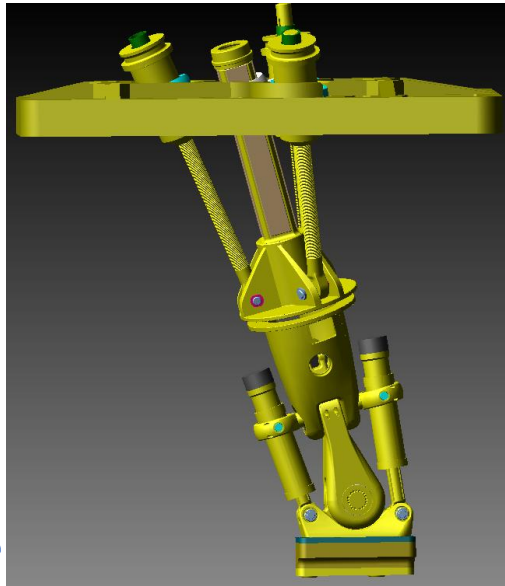
- *Developing the FE model of the whole W7X insulation system*
- *Modelling about 1000 connections between the insulation system and plasma vessel using APDL programming*
- *Performing Implicit Dynamic analysis*
- *EM analysis*



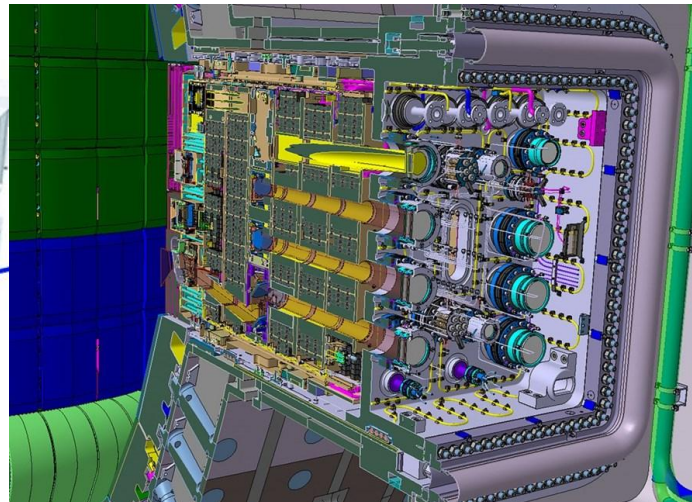
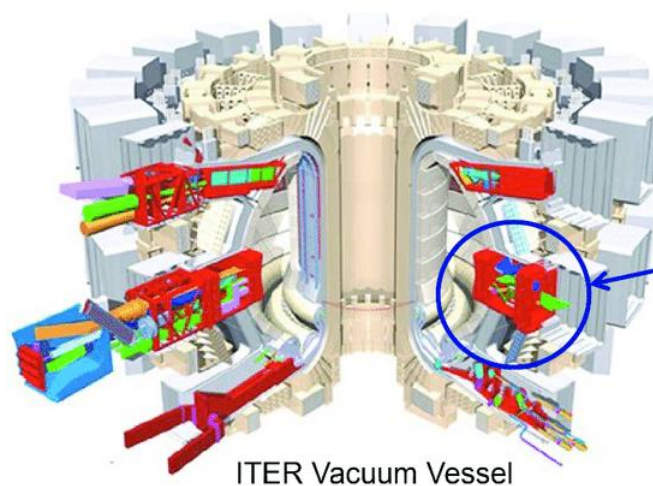
Connections created automatically by APDL programming

Multi-body simulation – load analysis with MSC ADAMS

- MBD simulation of mechanisms (remote maintenance systems, Nuclear plant)
- Extract loads to be used for structural analysis
- Predict the performance of the system (speed, power required, trajectory)
- Flexible bodies can be added, based on Abaqus FE modal analysis

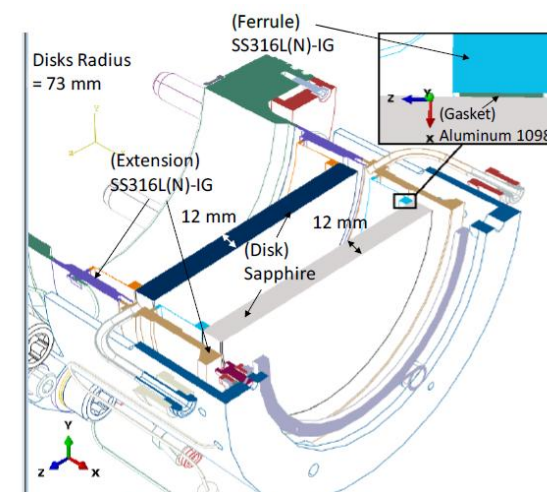
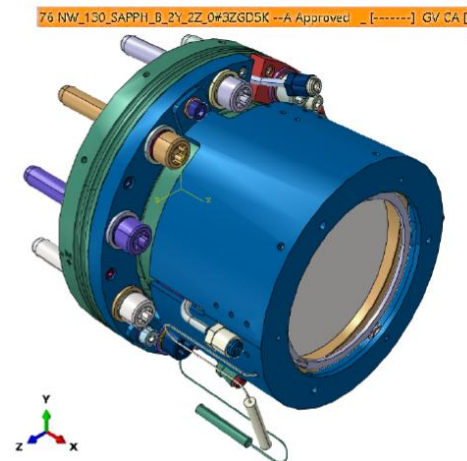
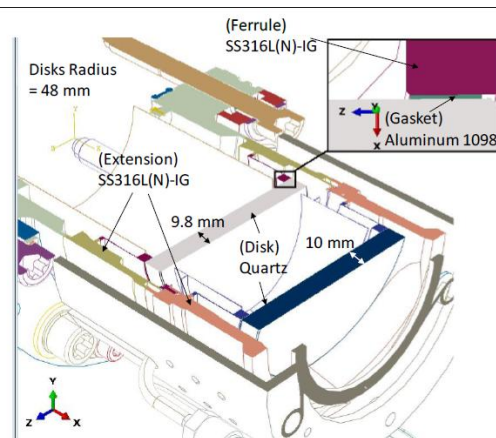
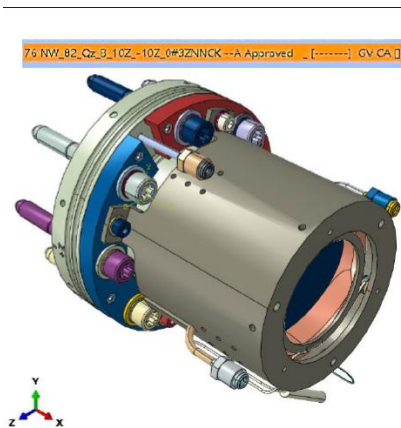


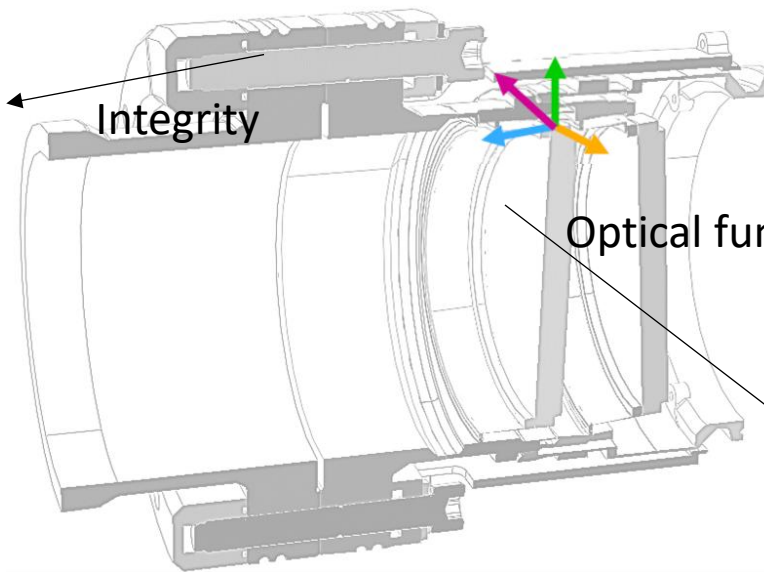
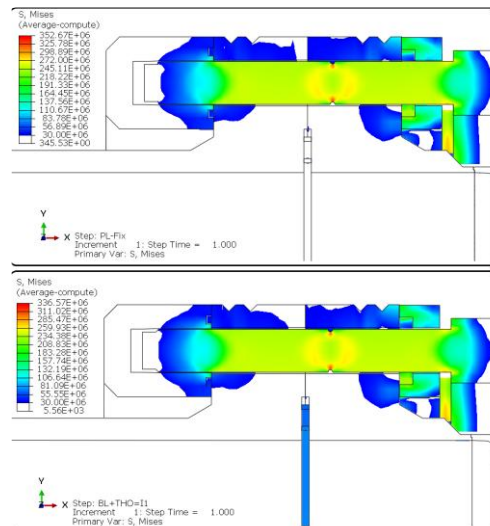
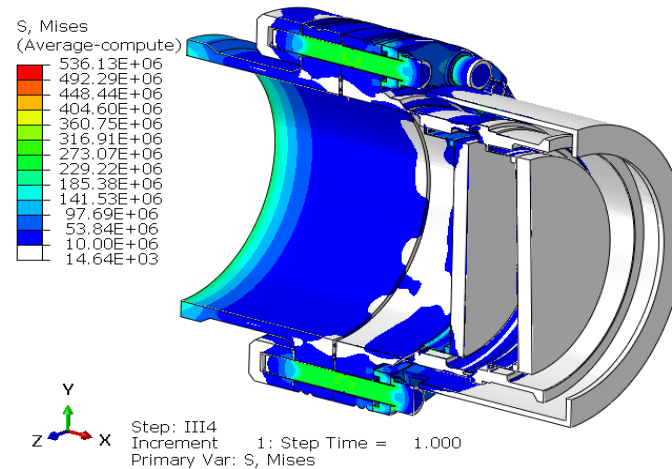
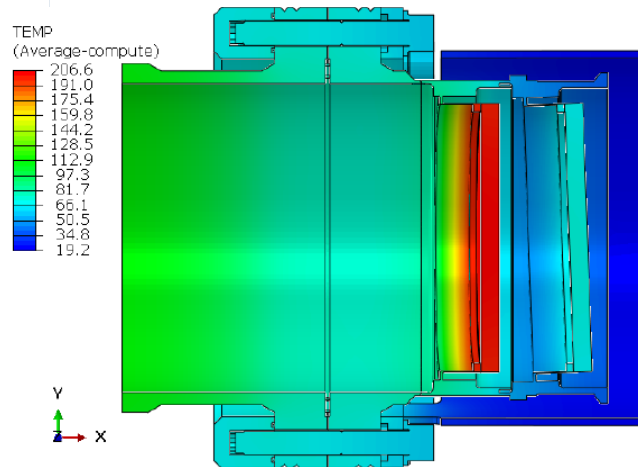
Multi-body application



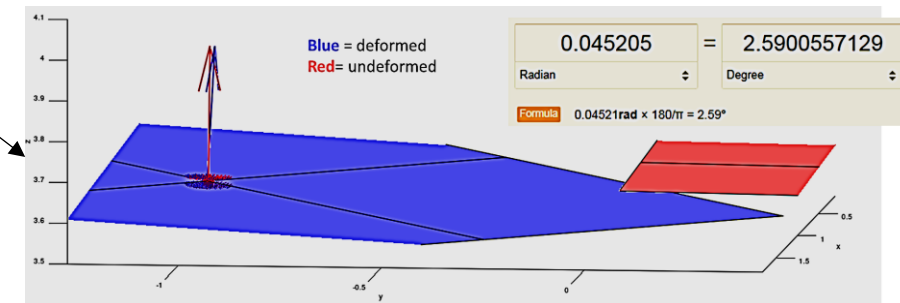
Precision optomechanical design by analysis for ensuring:

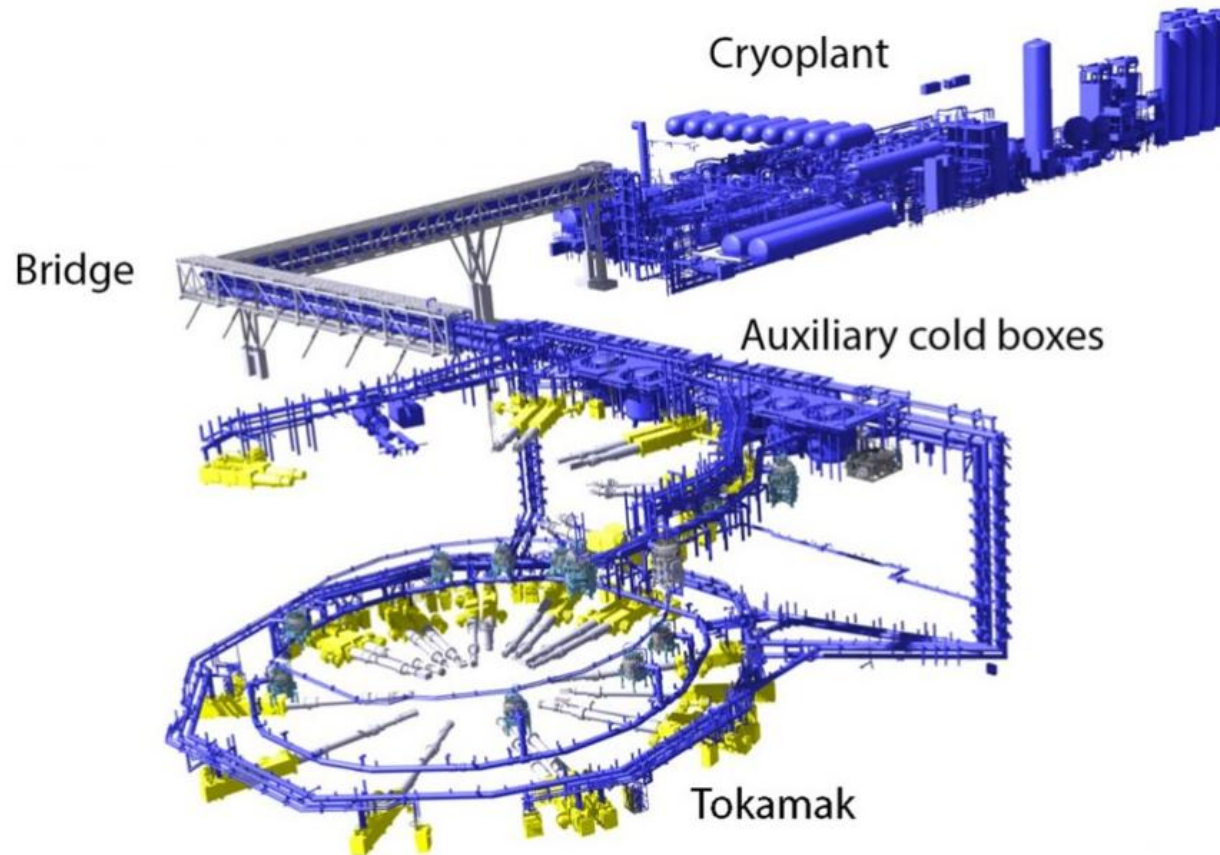
- ✓ No risk in manufacturing aftermath (glass-metal Diffusion Bonding)
- ✓ Vacuum and cleanliness maintainability facing cyclic loading
- ✓ Structural integrity and flanging leak-tightness facing plasma and disruption
- ✓ Thermal stability facing signal beams, lasers and other heats





- Orthotropic glass materials
- Multi-metallic cyclic plasticity
- Thermal shrinkage and expansion effects (assembly thermoelasticity mismatch)
- Subcomponents fatigue life
- Ratcheting and shakedown induced by beam and other loads
- Geometrical and material optimization for integrity and functionality

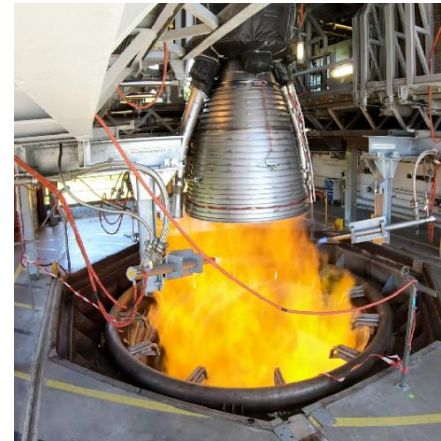




- Cryogenic system of the tokamak
- Thermal and Structural analysis
- Sub-models to verify all the joints and connections
- Structural assessment based on standards



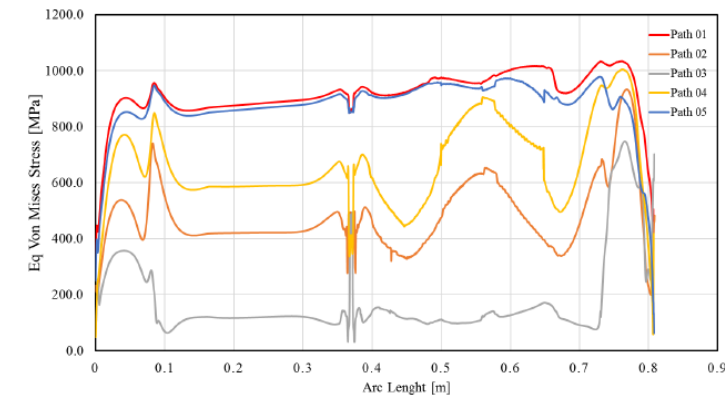
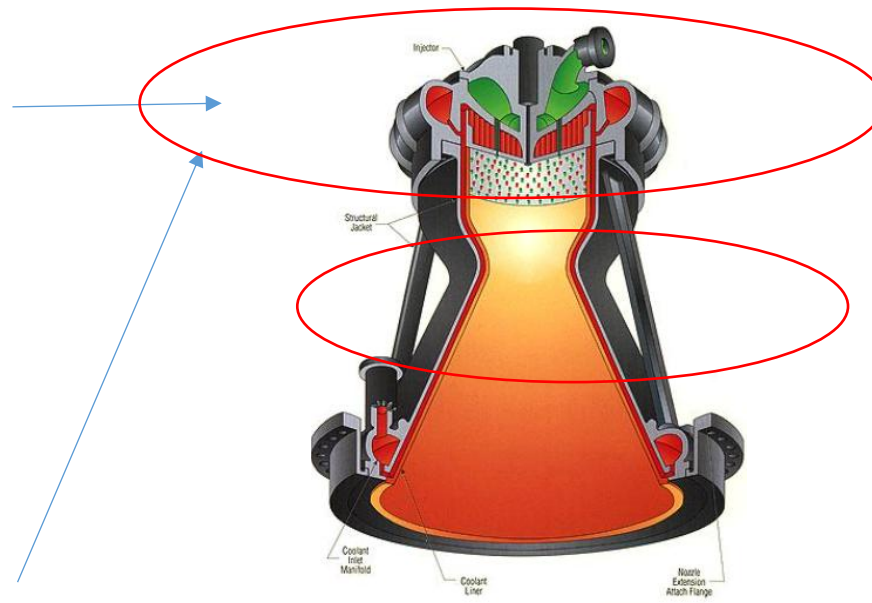
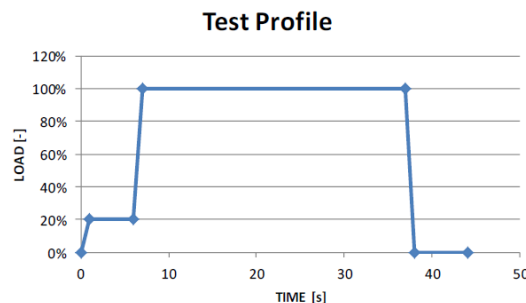
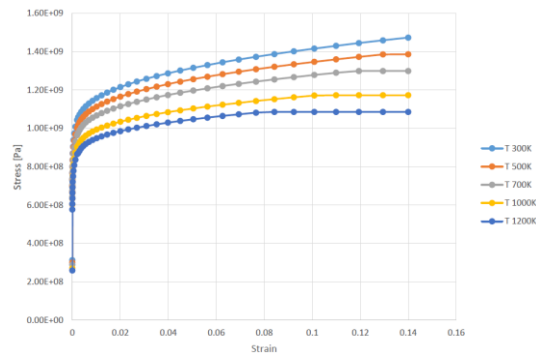
Rocket Engine Components



Launching System Components

Rocket engine injector head thermo-structural analysis

- Thermo-structural analysis of a section of the rocket engine of a small size launcher
- Firing test has been simulated by FE analysis
- Complex non-linear material physical properties and thermal interactions incorporated in the model
- Transient temperature field and stress distribution have been calculated
- Yield and Ultimate Safety factors calculated at every step of the simulation



Reference picture, real images are company confidential information that cannot be shown

Rocket Applications

Thermo-structural analysis of Ariane 6 launch site components

Rocket Applications

- Thermo-structural analysis 500 [s] test has been simulated by FE analysis
- Complex non-linear material physical properties and thermal interactions incorporated in the model
- Transient temperature field and stress distribution have been calculated



- **ITER Framework Service Contract IO/20/CT/6000000304 “Design Analysis for the ITER TOKAMAK Engineering”** – (2020-2028) – Capgemini Leader of the Consortium composed by Capgemini, LTCalcoli, ENEA Frascati, Università di Palermo.
- **ITER Framework Contract ITER IO/20/CT/6000000323 “Diagnostic Infrastructure Development and Engineering Service”**– (2020-2026)- Vitrociset Leader of the Consortium composed by Vitrociset, ENEA, ISTP, LTCalcoli, University Tor Vergata
- **ITER Framework Service Contract ITER/17/CT/6000000207 “Engineering Technical Support for Tokamak Engineering Department” Lot 1 – Design Supporting Analysis”** – (2017-2022) - LTCalcoli Leader of the Consortium composed by LTCalcoli, ENEA Frascati, Università di Palermo, Sogeti HT
- **ITER Framework Service Contract ITER IO/16/CT/SAP 6000000181 “Diagnostic Systems Engineering Services”**– (2016-2022)- Consortium composed by LTCalcoli, Vitrociset, IFP-CNR, RFX
- **ITER Contract n° IO/12/43-586: “Electromagnetic analysis Support”**– support to ITER EM analysis division in developing the ITER EM Global Model, Maxwell forces for different ferromagnetic components, EM dimensioning of In-vessel as Out- vessel components, EM loads on Cables and cable trays ... – (2012-2014)
- **EUROFUSION Contract: “EM, Thermo-mechanical Design analysis of the new DEMO Design Concept”**, (2014, 2010)
- **ITER Contract n° 43-599: “Engineering Support for Mechanical, Thermo-Hydraulic and Electromagnetic Analysis of the ITER Diagnostic Components”** – (2012-2017)
- **ITER Contract n° IO/CT/60-104: “Engineering Support to ITER Diagnostics”** – Support to ITER diagnostic Group in definition, performance, design and design analysis of ITER Diagnostics (2012- 2014)
- **ITER Contract n° ITER/CT/11/60-080: “Engineering Technical Support for the ITER TOKAMAK Directorate”** – EM, Thermal and Mechanical Analysis for the Design Assessment Analysis of ITER Vessel and In-Vessel components (2011- 2016)
- **ITER Contract n° ITER/08/382 Amd #1: “Analysis and optimization of the active and passive magnetic field reduction system of the ITER neutral beam injector”** –(2010-2011).
- **F4E Contract n° F4E-2008-OPE-06-06-08 (ES-AC) – Task 8: Electro-Mechanical analysis for Preliminary Design of three First Wall modules: Blk 2, 10, 18.** (2011- 2012)
- **ITER Contract n° IO/10/43-318: “Design Analysis of various ITER Diagnostics components”** –(2011-2012)
- **ITER Contract n° IO/08/41-241: “Electromagnetic analysis for the In-Wall Shielding”** – Evaluation of eddy currents and related EM forces for In-Wall Shielding blocks in Special Configuration during plasma disruption events. – (2008-2009)

- F. Lucca et al., *Detailed Electromagnetic Analyses of the ITER in Vessel Components during Plasma Disruptions*, 17th IEEE/NPSS Symposium on Fusion Engineering, October 6-10, 1997, San Diego, CA, USA
- Ferrari, W Daenner, M. Roccella et al. *The European Breeding Blanket Design for ITER* 17th/NPSS Symp. On Fusion Engineering - San Diego, CA, 6-10 – October 1997
- F. Lucca, M. Roccella et al, *Impact of the D-Shaped Plasmas on the new Limiters and on the Vacuum Vessel of FTU*, ISFNT5 (1999)
- F. Lucca et al, ITER reference breeding blanket design, Fusion Engineering and Design, Volume 46, Issues 2-4, November 1999, Pages 177-183
- F. Lucca, M. Roccella et al, Design of a welded box divertor cassette for ITER FEAT, Fusion Engineering and Design, Volumes 56-57, October 2001, Pages 239-242
- F. Lucca et al, Numerical simulation of welds of thick steel sheets for some experimental models towards ITER TF coil case, Fusion Engineering and Design, Volumes 58-59, November 2001, Pages 231-236
- F. Lucca, M. Roccella et al, Design of plasma facing components for the ITER feat divertor, Fusion Engineering and Design, Volumes 61-62, November 2002, Pages 153-163
- F. Lucca et al., Dual coax feed (32 and 8.4 GHZ) for Doppler tracking of the Cassini mission, from the primary focus of VLBI antennas, 25th ESA Antenna Workshop on Satellite Antenna Technology, 18-20 September 2002, ESTEC, Noordwijk, Holland
- F. Lucca, M. Roccella et al, EM Issues on the ITER-FEAT In-Vessel Components during Plasma Disruptions, SOFT 2002
- F. Lucca, M. Roccella et al, Plasma Chamber of the IGNITOR Machine, APS, New Mexico October 27-31 2003
- F. Lucca, M. Roccella et al, First Wall of the IGNITOR Machine, APS, New Mexico October 27-31 2003
- F. Lucca, M. Roccella et al. Disruption Scenarios and their Effects on the Ignitor First Wall. American Physical Society, 45th Annual Meeting of the Division of Plasma Physics, October 27-31, Albuquerque, New Mexico (2003)
- F. Lucca, M. Roccella et al, Design Modification of Plasma Facing Component and Cassette Body for ITER Divertor, SOFE (2003), October 14-17, San Diego, CA, USA
- F. Lucca, M. Roccella et al, Design of Plasma Chamber for IGNITOR Tokamak, SOFE (2003), October 14-17, San Diego, CA, USA
- F. Lucca et al, Proposal of litization of FTU vacuum vessel by using a Lithium Limiter, SOFT 23, 20-24 September 2004, Venice, Italy
- F. Lucca, M. Roccella et al, Preliminary analysis on a liquid lithium limiter in capillary porous system (CPS) configuration in view of a “litization” experiment on FTU tokamak, Fusion Engineering and Design, Volumes 75-79, November 2005, Pages 351-355
- F. Lucca, M. Roccella et al. Plasma Chamber and First Wall IGNITOR Experiment. American Physical Society, (2005)
- F. Lucca, M. Roccella et al. Remote Handling System IGNITOR. American Physical Society,(2005)
- F. Lucca, M. Roccella et al, Ignitor plasma chamber structural design with dynamic loads due to plasma disruption event, Fusion Engineering and Design, F. Lucca, M. Roccella, A. Marin et al. Ignitor Vacuum Vessel structural design with dynamic loads due to plasma disruption event, Fusion Engineering and Design, Volumes 75-79, November 2005, Pages 511-517



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